

(1)



Europäisches Patentamt
European Patent Office
Office européen des brevets



(11) Publication number:

0 655 508 A1

(12)

EUROPEAN PATENT APPLICATION

(21) Application number: 93119268.6

(51) Int. Cl.⁶: **C21C 5/52, C21C 5/54**

(22) Date of filing: **30.11.93**

(43) Date of publication of application:
31.05.95 Bulletin 95/22

(84) Designated Contracting States:
AT BE DE ES FR GB NL SE

(71) Applicant: **CENTRO SVILUPPO MATERIALI
S.p.A.**
Via di Castel Romano 100/102
I-00128 Roma (IT)

(72) Inventor: **Masucci, Pasquale**
Via della Pisana, 193
I-00163 Roma (IT)

(74) Representative: **Gervasi, Gemma, Dr. et al**
Studio Brevetti e Marchi
NOTARBARTOLO & GERVASI S.r.l.
33, Viale Bianca Maria
I-20122 Milano (IT)

(54) **Process for using foamed slag in stainless steel production in the electric arc furnace.**

(57) In the production of stainless steels in electric arc furnaces, it is possible to use foamed slag, with great advantages, by using a metal charge with specific carbon and silicon contents, by insulating limestone and carbon, by controlling the amount of employed oxygen and by maintaining basicity index of the slag within the range of 1,4 to 2.

EP 0 655 508 A1

Field of the invention

The present invention relates to a process for using foamed slag in stainless steels production and more specifically concerns the reduction of consumption of power, of wall refractory, of the furnace and of the electrodes, as well as the output increase and the production optimization by means of using foamed slag.

Prior art

In steel production with electric furnace, the furnace itself is filled up with metal scrap of suitable composition, the electrodes are lowered and the electric current starts to flow. The scrap just below the electrodes is melted first and the electrodes are lowered accordingly. When the electrodes are in their standard working position a great amount of not yet molten metal surrounds them, interposing between them and the furnace walls, which are thus sheltered from the radiation of arcs, which are at a temperature ranging between 6,000 and 10,000 °C, a temperature much higher than the one the refractory material constituting the walls of the furnace can resist to.

However, when a large amount of scrap is molten, the walls are no longer sheltered and are thus exposed to the destroying action of the radiation of arcs.

Such drawback was traditionally amended by reducing the furnished electric power, by lowering the voltage to the electrodes and by shortening the length of the electric arcs, which thus were, at least partially, sheltered by the slag thickness, which is naturally present on the surface of the metallic molten bath. Such action saves the refractory but lengthens the treating times in the furnace and increases the electrodes and energy consumption.

In the production of carbon steels with electric furnace it has been introduced since a long time the use of the so called foamed slag by introducing carbon or coke in the slag onto the bath and oxygen in the bath itself: the first reduces iron oxide to iron, thus producing carbon oxide, while oxygen reacts with the carbon in the bath thus forming further carbon oxide. Such a gas, by bubbling through the slag layer, let it foam and thus largely increases its volume. The foamed slag envelops the electrodes and interposes between the electric arcs and the walls of the furnace.

It is thus possible to keep the arc power to maximum values by using very high voltage with lower currents and longer arcs, with a consequent increase of furnace output, lower thermic losses, lower consumption of electrodes and electric power.

However, the technique of the foamed slag has not found an application in stainless steels production, essentially because during their melting the amount of iron oxide in the slag, typically around 1-3%, is largely insufficient to produce foamed slags, and because the oxygen insufflation produces chromium oxidation, thus arising the need of further additions of it, which turns into an increase of production costs.

Furthermore, the quite high amount of chromite and the very low amount of iron oxide renders the slag scarcely fluid and omogeneous and produces not perfectly molten aggregates having various dimensions, thus preventing in any case the foaming.

In consequence, the present state of the art expressly denies the possibility of using foamed slag in the production of stainless steels, only allowing to obtain a balance, within certain limits, between the reduction of the consumption of the walls of the furnace and the increase of the production costs due to electric power and to electrodes consumption increase.

Summary of the invention

The purpose of the present invention is to allow the use of foamed slag in the stainless steels production.

A further purpose of the present invention is to optimize the stainless steels production by increasing the working period of the furnace by reducing the wall consumption, as well as reducing the electrodes and electric power consumption.

Another purpose of the present invention is to reduce the production costs by reducing chromium oxidation in the metallic bath. A further purpose of the present invention is to increase the process output.

Detailed description of the invention

The process according to the present invention for using foamed slag in the production of stainless steels from electric furnace molten baths is characterized by the co-operation of the following operative steps:

- to put into the furnace a charge comprising scrap, a Fe-Si alloy, a Fe-Cr alloy and at least a component selected from carbon and coke;
- to put into the slag a mixture of at least a component selected from carbon and coke with limestone, with a ratio limestone/carbon in the mixture ranging between 0.1 and 5;
- to maintain in said charge the total amounts of carbon and silicon respectively ranging between 0.7 and 2.5 and between 0.6 and 1.1% by weight, in any case as a function of

the amount of the blown oxygen:

- to insufflate oxygen with a flow rate ranging between 15 and 30 Nm³/h per ton of steel in the bath and in amount ranging between 5 and 20 Nm³ per ton of steel;
- to maintain the basicity index of the slag within values ranging between 1.4 and 2;

the further process steps is the usual one employed for the stainless steels production.

It is possible to add carbon and silicon amounts higher than those indicated if it is possible to operate with higher amounts of insufflated oxygen and, above all, if it is possible to finish the production process with high carbon amounts inside the bath, however under normal working conditions the above mentioned values of carbon and silicon amounts, as well the amounts of used oxygen have proved perfectly suitable.

Carbon and silicon amounts lower than the ones indicated cannot avoid the chromium overoxidation, particularly when high oxygen amounts are blown, whereas higher carbon amounts need too long treating times in the electric furnace or in the further treatment in AOD furnace for their removal.

Higher silicon values involve too low basicity indexes with consequent erosion of the electric furnace refractory, namely the need to counterbalance them with further additions of calcium oxide, and the subsequent waste of energy for its melting.

Oxygen amounts as indicated are suitable for a standard production, even though it is possible to change them to comply with particular process conditions which are going to be used; however it must be taken into consideration that, in any case, consumptions higher than the ones mentioned above must be adequately counterbalanced by higher carbon additions to the bath, at least producing a increase of costs.

The oxygen insufflation begins as soon as a suitable amount of liquid bath is formed and naturally it contributes to minimize the electric power consumption, owing to the heat developed during combustion, mainly by carbon.

As far as the basicity index is concerned, it is noted that even though slightly higher values than the ones indicated can however be used, much higher values lead to too dense slags which hardly foam, while values lower to the minimum indicated above produce, as hinted, attacks to the furnace refractory.

The slags produced according to the invention foam easily and well, owing to the carbon oxide produced by the following reactions: i) combustion of the carbon dissolved in the bath, ii) between the carbon added as carbon and/or coke and the chromite, in the slag, iii) between limestone and carbon, in the slag.

It is to be noted that the carbon and silicon added protect chromium from oxidation.

The vigorous mixing of the slag induced by the bubbling of carbon oxide promotes its homogenization and its quick complete melting, thus improving the inherent characteristics suited for a good foaming. Such effect is improved in that chromium oxide not dissolved in the slag, liquid near to the electric arc, is diffused in all the slag and far from the arc it solidifies in the shape of very little crystals which contribute to stabilize the foamed layer of the slag itself.

Carbon (or coke) and limestone can be added basically in two ways:

- pneumatic insufflation in the slag by means of a specific duct inserted i.e. through the scorification port of the furnace, as a mixture with granular size ranging between 0.01 and 5 mm;
- introduction from the 5th opening of the vault furnace, as ovules consisting in part of carbon or coke and limestone and in part of carbon or coke alone.

By operating according to the above teaching, the aforementioned advantages can be reached. The foamed and firm slag protects the refractory from erosion caused by the exposure to the irradiation of the electric arc; it is thus possible to keep the arc long, lowering the current and minimizing the electric power consumption; as a consequence it is minimized the consumption of the electrodes; the chromium losses are reduced; the production times and productivity are optimized.

EXAMPLE

The present invention will be now described in connection with a practical production test in an industrial plant with a charge (consisting of 140 ton of stainless steel scrap and carbon steel, of chromium iron alloy and of 5 ton of calcium oxide) with the following % by weight content of the more interesting elements according to the invention:

C 0.9; Si 0.8; Cr 18;

and introduced into the furnace with two subsequent additions, called "baskets".

The first basket consisted of 75 ton of scrap with C and Si amounts respectively of 0.4 and 0.8 % b.w., and of 2 ton of CaO.

After supply of 100 kWh/t, a mixture consisting in 600 kg of carbon, with 70% b.w. of C, and 500 kg ovules consisting in limestone for 40% b.w. and coke for 60% b.w., 85% b.w. in C, with granular size ranging between 0.1 and 2 mm. was added through the 5th opening of the vault furnace. The flow rate of this addition was 100 kg/min. After two minutes from the starting of addition of ovules, the foaming of the slag started.

To the second basket, weighing 65 ton of scrap, with C and Si amounts respectively of 1.4 and 0.75% b.w., after supply of 70 kWh/t, 500 kg of Fe-Si at 65% were added from the 5th opening. At about 100 kWh/t a mixture consisting in 1000 kg of carbon, at 70% b.w. of C, and 1000 kg of ovules of limestone and coke were added, as indicated for the first basket, with a flow rate of 100 kg/min. At about 250 kWh/t the foaming became excessive; as a consequence the flow rate of the mixture was lowered to 60 kg/min and the furnace was slightly tilted to prevent the foam to come out of the scorification port.

400 Nm³ oxygen were insufflated in the first basket with flow rate of 2500 Nm³/h; 1600 Nm³ oxygen were insufflated in the second basket with flow rate of 3200 Nm³/h.

The basicity index at the end of the castings was 2.

The advantages obtained in terms of consumption of refractory, of electrodes, of electric power, of output, of chromium yield after a series of castings performed according to the described teachings and in any case within the limits of the present invention, can be thus summed up:

- Reduction of power consumption: 5%;
- Reduction of refractory consumption: 44%;
- Reduction of consumption of electrodes: 15%;
- Increasing in productivity: 22%;
- Increasing in chromium yield: 23%;

Claims

1. Process for using foamed slag in the production of stainless steels in electric arc furnace, characterized by the co-operation of the following steps:
 - to put into the furnace a charge comprising scrap, a Fe-Cr alloy, a Fe-Si alloy and at least a component selected from carbon and coke, maintaining carbon and silicon total amounts respectively ranging between 0.7 and 2.5 and between 0.6 and 1.1% b.w.;
 - to put into the slag a mixture of at least a component selected from carbon and coke with limestone, with a ratio limestone/carbon in the mixture ranging between 0.1 and 5 and granular size ranging between 0.01 and 5 mm;
 - to insufflate oxygen with a flow rate ranging between 15 and 30 Nm³/h per ton of steel in the bath and in amount ranging between 5 and 20 Nm³ per ton of steel;
 - to maintain the basicity index of the slag within values ranging between 1.4 and 2.



European Patent
Office

EUROPEAN SEARCH REPORT

Application Number
EP 93 11 9268

| DOCUMENTS CONSIDERED TO BE RELEVANT | | | |
|---|---|---|--|
| Category | Citation of document with indication, where appropriate, of relevant passages | Relevant to claim | CLASSIFICATION OF THE APPLICATION (Int.Cl.6) |
| A | PATENT ABSTRACTS OF JAPAN vol. 13, no. 504 (C-653)13 November 1989 & JP-A-01 201 415 (SUMITOMO METAL IND LTD) 14 August 1989 * abstract * | | C21C5/52 C21C5/54 |
| A | PATENT ABSTRACTS OF JAPAN vol. 12, no. 263 (C-514)22 July 1988 & JP-A-63 047 351 (SANYO TOKUSHO SEIKO KK) 29 February 1988 * abstract * | | |
| A | FR-A-2 634 787 (INSTITUT DE RECHERCHE DE LA SIDERURGIE FRANCAISE, IRSID) | | |
| A | EP-A-0 162 679 (METRO MATERIALS CORPORATION) | | |
| | | | TECHNICAL FIELDS SEARCHED (Int.Cl.6) |
| | | | C21C |
| The present search report has been drawn up for all claims | | | |
| Place of search THE HAGUE | | Date of completion of the search 22 April 1994 | Examiner Oberwalleney, R |
| CATEGORY OF CITED DOCUMENTS | | | |
| X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application I : document cited for other reasons * : member of the same patent family, corresponding document | | | |

EPO FORM 1503 (12.1) (P/0004)

